# Optical trapping forces of focused circular partially coherent beams on Rayleigh particles 

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#### Abstract

The optical trapping forces of tightly-focused radially polarized circular partially coherent beams on Rayleigh particles are theoretically investigated. Numerical calculations are performed to study the optical trapping forces on Rayleigh particles for different initial coherent length of the incident circular partially coherent beams. The results show that the magnitude of the gradient force decreases with the reduction of the initial coherent length of the focused radially polarized circular partially coherent beams, while the balanced position (i.e., the position where the optical trapping forces becomes zero) stays constant. Moreover, the focused spot gradually elongates along the optical axis with the reduction of the initial coherent length, and the axial gradient force on Rayleigh particles also decreases gradually with the reduction of the intensity gradient in axial direction. As there exists an spherical aberrant in the focusing optical system, the focal spot in the direction of the optical axis becomes trumpet-shaped, and the optical trapping forces on Rayleigh particles change as well.


Keywords: tight focusing, radially polarized, circular partially coherent, spherical aberration, optical trapping force.

## 1. Introduction

Subwavelength focal patterns can be generated by focusing laser beams with a high numerical aperture (NA) objective [1-3]. With proper modulation on the phase and polarization of the incident beam, the patterns can be controlled, which have found applications in optical data storage, microscopy, particle beam trapping and material processing [4-11]. Extensive research efforts on tightly focused phase or polarization modulated beams have been carried out for decades [8]. The coherence property of light offers another degree for intensity modulation of tightly focused field. Previous
studies indicated that the spatial coherence of a partially coherent beam apparently influences the evolution behaviors of spectral density, degree of coherence, and state of the polarization [12-15].

On the other hand, significant advances have been achieved recently in designing and producing nonconventional correlation sources. Some novel partially coherent beams with peculiar correlation functions have been introduced, which exhibit nontrivial propagation properties such as far-field flat-topped, ring-shaped, self-focusing, self-splitting, optical cage and optical lattices [16-19]. For example, Santarsiero and his collaborators recently introduced the circular partially coherent light beams, which exhibits perfect coherence along any annulus but partial or even vanished coherence between two points with different radial distances [20,21]. Ding et al. demonstrated the self-focusing property of such beam on propagation in oceanic turbulence [21]. Lin and his collaborators found that an optical needle with adjustable length along the optical axis can be obtained by regulating the coherent length of incident circular partially coherent beams [22,23]. Such non-diffracting optical needle may have potential applications in atom trapping, living biological cells manipulating, materials processing. To investigate the mechanical effect of circular partially coherent beams in a tightly focused scheme, the optical trapping forces of radially polarized circular partially coherent beams on Rayleigh particles are studied in this paper. In particular, since optical microscopes are commonly plagued by the aberrations, such as spherical aberration, defocus, and astigmatism etc. As an example, the effect of spherical aberration of the focusing system on the optical trapping force is also discussed.

## 2. Theoretical analysis

In this study, radially polarized circular partially coherent beams are employed as the incident laser beam, the cross-spectral density of the focal field formed by a high NA objective can be expressed as [23]

$$
\begin{align*}
W_{0}\left(\mathbf{r}_{1}, \mathbf{r}_{2}\right) & =\frac{I_{0}}{w_{0}^{2}} \exp \left(-\frac{r_{1}^{2}+r_{2}^{2}}{w_{0}^{2}}\right)\left[\begin{array}{ll}
\operatorname{sinc}\left(\frac{r_{2}^{2}-r_{1}^{2}}{\delta^{2}}\right) x_{1} x_{2} & \operatorname{sinc}\left(\frac{r_{2}^{2}-r_{1}^{2}}{\delta^{2}}\right) x_{1} y_{2} \\
\operatorname{sinc}\left(\frac{r_{2}^{2}-r_{1}^{2}}{\delta^{2}}\right) y_{1} x_{2} & \operatorname{sinc}\left(\frac{r_{2}^{2}-r_{1}^{2}}{\delta^{2}}\right) y_{1} y_{2}
\end{array}\right] \\
& =\frac{E_{0}^{2}}{w_{0}^{2}} \exp \left(-\frac{r_{1}^{2}+r_{2}^{2}}{w_{0}^{2}}\right) \operatorname{sinc}\left(\frac{r_{2}^{2}-r_{1}^{2}}{\delta^{2}}\right)\left[\begin{array}{ll}
x_{1} x_{2} & x_{1} y_{2} \\
y_{1} x_{2} & y_{1} y_{2}
\end{array}\right] \tag{1}
\end{align*}
$$

In Eq. (1) $, \operatorname{sinc}(x)=\sin (x) / x, w_{0}$ is the beam width, $\delta$ is the initial coherent length, $\mathbf{r}=(r, \varphi)$ is the position vector at the source plane, $E_{0}$ is the characteristic amplitude
of incident beam, and $I_{0}$ is the intensity of incident beam. It should be noted that the variables $\mathbf{r}_{1,2}$ in $W_{0}\left(\mathbf{r}_{1}, \mathbf{r}_{2}\right)$ are position vectors, while the other $r_{1,2}$ in Eq. (1) are scalars, because the cross-spectral density of radially polarized circular partially coherent beams is angle-independent. Additional, $r_{1,2}$ and $\psi_{1,2}$ are the magnitude and the angle in polar coordinates at the plane of incidence, respectively. $x_{1,2}$ and $y_{1,2}$ are the abscissa and the ordinate in Cartesian coordinates at the plane of incidence, respectively. Under the sine condition [24], i.e., $r=f \sin \theta$, where $f$ is the focal length of the objective, the two point pupil apodization correlation function of the incident beam can be expressed as [22]

$$
\begin{align*}
F\left(\varphi_{1}, \varphi_{2}, \theta_{1}, \theta_{2}\right) & =\exp \left(-\frac{r_{1}^{2}+r_{2}^{2}}{w_{0}^{2}}\right) \operatorname{sinc}\left(\frac{r_{2}^{2}-r_{1}^{2}}{\delta^{2}}\right) \\
& =\exp \left[-\frac{f^{2}\left(\sin ^{2} \theta_{1}+\sin ^{2} \theta_{2}\right)}{w_{0}^{2}}\right] \operatorname{sinc}\left[\frac{f^{2}\left(\sin ^{2} \theta_{2}-\sin ^{2} \theta_{1}\right)}{\delta^{2}}\right] \tag{2}
\end{align*}
$$

As the beam focused by a high NA objective, the second-order correlation properties of the focal field can be characterized by a $3 \times 3$ electric cross-spectral density matrix $W\left(\boldsymbol{\rho}_{1}, \boldsymbol{\rho}_{2}, \mathbf{z}\right)$ [25]. In this study, after some tedious integration, the elements of the $3 \times 3$ matrix in the focal region can be obtained as follows:

$$
\begin{align*}
& W_{i j}\left(\rho_{1}, \rho_{2}, \psi_{1}, \psi_{2}, z\right)=4 I_{0}\left(\frac{\pi}{\lambda}\right)^{2} \int_{0}^{\alpha} \int_{0}^{\alpha} \frac{f^{2}}{w_{0}^{2}} \cos ^{3 / 2} \theta_{1} \cos ^{3 / 2} \theta_{2} \\
& \quad \times \exp \left[-\frac{f^{2}\left(\sin ^{2} \theta_{1}+\sin ^{2} \theta_{2}\right)}{w_{0}^{2}}\right] \operatorname{sinc}\left[\frac{f^{2}\left(\sin ^{2} \theta_{2}-\sin ^{2} \theta_{1}\right)}{\delta^{2}}\right] \\
& \quad \times \exp \left[i k z\left(\cos \theta_{2}-\cos \theta_{1}\right)\right] \exp \left[-i k \beta f^{4}\left(\sin ^{4} \theta_{1}-\sin ^{4} \theta_{2}\right)\right] \\
& \quad \times M_{i j}\left(\rho_{1}, \rho_{2}, \psi_{1}, \psi_{2}, \theta_{1}, \theta_{2}\right) \mathrm{d} \theta_{1} \mathrm{~d} \theta_{2} \tag{3}
\end{align*}
$$

$$
(i, j=x, y, z)
$$

In Eq. (3), $\beta$ is the spherical aberration coefficient, and $M_{i j}\left(\rho_{1}, \rho_{2}, \psi_{1}, \psi_{2}, \theta_{1}, \theta_{2}\right)$ for the elements on the primary diagonal of the $W\left(\boldsymbol{\rho}_{1}, \boldsymbol{\rho}_{2}, \mathbf{z}\right)$ are

$$
\begin{align*}
& M_{x x}\left(\rho_{1}, \rho_{2}, \psi_{1}, \psi_{2}, \theta_{1}, \theta_{2}\right) \\
& \quad=J_{1}\left(k \rho_{1} \sin \theta_{1}\right) J_{1}\left(k \rho_{2} \sin \theta_{2}\right) \sin ^{2} \theta_{1} \sin ^{2} \theta_{2} \cos \psi_{1} \cos \psi_{2}  \tag{4}\\
& \begin{aligned}
M_{y y}\left(\rho_{1},\right. & \left.\rho_{2}, \psi_{1}, \psi_{2}, \theta_{1}, \theta_{2}\right) \\
& =J_{1}\left(k \rho_{1} \sin \theta_{1}\right) J_{1}\left(k \rho_{2} \sin \theta_{2}\right) \sin ^{2} \theta_{1} \sin ^{2} \theta_{2} \sin \psi_{1} \sin \psi_{2}
\end{aligned}
\end{align*}
$$

$$
\begin{align*}
& M_{z z}\left(\rho_{1}, \rho_{2}, \psi_{1}, \psi_{2}, \theta_{1}, \theta_{2}\right) \\
& \quad=J_{0}\left(k \rho_{1} \sin \theta_{1}\right) J_{0}\left(k \rho_{2} \sin \theta_{2}\right) \sin ^{3} \theta_{1} \sin ^{3} \theta_{2} \sin \psi_{1} \tag{6}
\end{align*}
$$

where $J_{0}$ and $J_{1}$ in Eqs. (4)-(6) are the zero-order and first-order Bessel functions of the first kind, respectively. By setting $\rho_{1}=\rho_{2}=\rho$ and $\psi_{1}=\psi_{2}=\psi$, the intensity of transverse polarized component of radially polarized circular partially coherent beams with negative spherical aberration in the focal region can be expressed as

$$
\begin{align*}
& I_{\text {transverse }}\left(\rho_{1}, \rho_{1}, \psi_{1}, \psi_{1}, z\right) \\
& \quad=W_{x x}\left(\rho_{1}, \rho_{1}, \psi_{1}, \psi_{1}, z\right)+W_{y y}\left(\rho_{1}, \rho_{1}, \psi_{1}, \psi_{1}, z\right) \tag{7}
\end{align*}
$$

and the $z$-polarization component, i.e., axial polarized light beams, is

$$
\begin{equation*}
I_{z}\left(\rho_{1}, \rho_{1}, \psi_{1}, \psi_{1}, z\right)=W_{z z}\left(\rho_{1}, \rho_{1}, \psi_{1}, \psi_{1}, z\right) \tag{8}
\end{equation*}
$$

The total intensity distribution in the focal region is

$$
\begin{align*}
& I_{\text {total }}\left(\rho_{1}, \rho_{1}, \psi_{1}, \psi_{1}, z\right) \\
& \quad=I_{x}\left(\rho_{1}, \rho_{1}, \psi_{1}, \psi_{1}, z\right)+I_{y}\left(\rho_{1}, \rho_{1}, \psi_{1}, \psi_{1}, z\right)+I_{z}\left(\rho_{1}, \rho_{1}, \psi_{1}, \psi_{1}, z\right) \tag{9}
\end{align*}
$$

In order to calculate the optical trapping force of radially polarized circular partially coherent beams with negative spherical aberration on nano- or micro-sized particles, for simplicity, it is assumed that the radius of the trapped particle is much smaller than the wavelength of the trapping laser, i.e., the particle can be treated as a point dipole and Rayleigh scattering occurs. With this assumption, the gradient and scattering forces of the particle can be separated and expressed respectively as [26]

$$
\begin{align*}
& \mathbf{F}_{\mathrm{g}}(\rho, z)=2 \pi a^{3} \frac{n_{2}}{c} \frac{m^{2}-1}{m^{2}+2} \nabla I(\rho, z)  \tag{10}\\
& \mathbf{F}_{\mathrm{s}}(\rho, z)=\frac{8}{3} \pi k^{4} a^{6} \frac{n_{2}}{c}\left(\frac{m^{2}-1}{m^{2}+2}\right)^{2} I(\rho, z) \tag{11}
\end{align*}
$$

In Eqs. (10) and (11), $a$ is the radius of the trapped particle, $k$ is the wave-number, $n_{2}$ denotes the refractive index of the particle, $n_{1}$ denotes the refractive index of the ambient medium, $m=n_{2} / n_{1}$, and $c$ is the speed of light in vacuum. Obviously, the gradient force $\mathbf{F}_{\mathrm{g}}$ is proportional to the intensity gradient and points up the gradient when $n_{2}>n_{1}$, and the scattering force $\mathbf{F}_{\mathrm{s}}$ is proportional to the light intensity.

## 3. Results and discussions

For the focusing system without spherical aberration, i.e., $\beta=0$, the beam waists of the focused radially polarized circular partially coherent beams lie in the geometric


Fig. 1. Normalized intensity distribution of radially polarized circular partially coherent beams in the geometric focal plane of a high NA objective for different $\delta$, (a) $\delta=w_{0}$, (b) $\delta=0.6 w_{0}$, and (c) $\delta=0.2 w_{0}$. The other calculation parameters are chosen as $\lambda=633 \mathrm{~nm}, w_{0}=5 \mathrm{~mm}, \mathrm{NA}=0.8, f=1 \mathrm{~cm}$, and $I_{0}=$ $=100 \mathrm{~mW} / \mu \mathrm{m}^{2}$ and $\beta=0$.
focal plane of the high NA objective. Figure 1 shows the total intensity distributions of radially polarized circular partially coherent beams in the geometric focal plane of a high NA objective for different initial coherent length. It could be concluded that although the spot size of the total intensity diffuses gradually with the decrease of initial coherent length, the lateral dimension of the dark hollow keeps nearly invariant. Because the gradient force of the focused light beams on Rayleigh particle is proportional to the intensity gradient, the diffusion of the intensity distribution means a decrease of radial gradient force. The invariance of the dark hollow of the intensity distribution probably means that the balanced position, where the gradient force is zero, does not change with coherent length.

Figure 2(a) shows the radial scattering force of the focused radially polarized circular partially coherent beams on the Rayleigh particle, which is assumed to be spherical and has a radius of 20 nanometers. Figure 2(b) indicates the radial gradient force



Fig. 2. The curve of radial scattering force and radial gradient force in focal plane for different initial coherent length, (a) radial scattering force, (b) radial gradient force. The other calculation parameters are chosen as $\lambda=633 \mathrm{~nm}, w_{0}=5 \mathrm{~mm}, \mathrm{NA}=0.8, f=1 \mathrm{~cm}, n_{2}=1.5, n_{1}=1.3, I_{0}=100 \mathrm{~mW} / \mu \mathrm{m}^{2}, a=20 \mathrm{~nm}$, and $\beta=0$.
for different initial coherent length. A comparison between Fig. 2(a) and (b) demonstrates that both radial gradient force and radial scattering force reduce with the decrease of the initial coherent length, and the magnitude of radial scattering force is much smaller than the radial gradient force. Figure 2(b) shows that the balanced position, in geometric focal plane of the high NA objective, does stay constant as coherent length decreases.

Figure 3 presents the gradient force on Rayleigh particle which is represented by the red arrows, and the intensity distribution of the focused radially polarized circular partially coherent beams for different initial coherent length in $\rho-z$ plane. Obviously, the intensity distribution of the focused radially polarized circular partially coherent beams in focal region gradually stretches along the optical axis as the initial coherent length decreases. Accompanied by the elongation of light spot in focal region along


Fig. 3. Gradient force and intensity distribution in $\rho-z$ plane of the focusing radially polarized circular partially coherent beams for different initial coherent length, (a) $\delta=w_{0}$, (b) $\delta=0.6 w_{0}$, and (c) $\delta=0.2 w_{0}$. Red arrows represent the direction of the gradient force, and the length of the arrows indicates the magnitude of the gradient force. The other calculation parameters are chosen as $\lambda=633 \mathrm{~nm}, w_{0}=5 \mathrm{~mm}$, $\mathrm{NA}=0.8, f=1 \mathrm{~cm}, n_{1}=1.3, n_{2}=1.5, I_{0}=100 \mathrm{~mW} / \mu \mathrm{m}^{2}, a=20 \mathrm{~nm}$, and $\beta=0$.


Fig. 4. Gradient force and intensity distribution of radially polarized circular partially coherent beams with negative spherical aberration in $\rho-z$ plane near the focus. Red arrows represent the direction of the gradient force, and the length of the arrows indicates the magnitude of the gradient force. The calculation parameters are chosen as $\lambda=633 \mathrm{~nm}, w_{0}=5 \mathrm{~mm}, \mathrm{NA}=0.8, \beta=15 \times 10^{-4} \mathrm{~mm}^{-3}, f=1 \mathrm{~cm}, n_{1}=1.3$, $n_{2}=1.5, I_{0}=100 \mathrm{~mW} / \mathrm{\mu m}^{2}, a=20 \mathrm{~nm}$, and $\delta=0.3 w_{0}$.
the optical axis, the axial gradient force on Rayleigh particle, which is represented by the red arrows pointing along the optical axis, decreases gradually. As shown in Fig. 3(c), when the value of initial coherent length is $\delta=0.2 w_{0}$, the direction of the red arrows are all along the radius in the region of $-22 \lambda \leq z \leq 22 \lambda$, and $-2 \lambda \leq \rho \leq 2 \lambda$. It represents that when the value of initial coherent length is $\delta=0.2 w_{0}$, the axial gradient force can be regarded as zero in the region of $-22 \lambda \leq z \leq 22 \lambda$, and $-2 \lambda \leq \rho \leq 2 \lambda$.

The optical trapping force on nano- or micro-sized particles may be strongly influenced by the emerging aberrations. Thus, the effect of negative spherical aberration on the optical trapping force for Rayleigh particles is studied. When the spherical aberration of the focusing system is $\beta=15 \times 10^{-4} \mathrm{~mm}^{-3}$, the gradient force and intensity distribution of the focused radially polarized circular partially coherent beams in $\rho-z$ plane near the focus are illustrated in Fig. 4. Apparently, when the focal system exists, the spherical aberration of the intensity distribution in $\rho-z$ plane is stretched and becomes trumpet-shaped. In $\rho-z$ plane, there are three peaks of light intensity, and they locate at $A(\rho=0, z=-32 \lambda), B(\rho=0.8 \lambda, z=-13.6 \lambda)$, and $C(\rho=0.8 \lambda, z=-13.6 \lambda)$. The distribution of red arrows illustrates that these three points of the peak intensity are three balanced positions where the gradient forces are zero. Moreover, the axial gradient force is not equal to zero in the region of $-38 \lambda \leq z \leq-5 \lambda$, and $-1.5 \lambda \leq \rho \leq 1.5 \lambda$ as the spherical aberration of the focusing system is $\beta=15 \times 10^{-4} \mathrm{~mm}^{-3}$.

## 4. Conclusion

The optical trapping forces of tightly-focused radially polarized circular partially coherent beams on Rayleigh particles have been investigated theoretically through numerical calculations. The results demonstrate that the magnitude of the radial gradient force in focal plane decreases with the reduction of the initial coherent length of the focused radially polarized circular partially coherent beams, while the balanced position stays constant. The axial gradient force on Rayleigh particles also decreases gradually with the reduction of the initial coherent length. As there exists an spherical
aberrant in the focusing optical system, the focal spot in the axial direction becomes trumpet-shaped and the axial gradient force is no longer equal to zero.

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